

Statistical-Mechanical Theory of the Deformation Dependence of Topological Constraints in Polymer Networks

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Summary

This paper describes a simple model of topological constraints on polymer network chains. In the frame of this model we calculate the deformation dependence of the constraining potential used in a theory of stress-strain behaviour previously.

Introduction

An extension of ideas of EDWARDS /1/ concerning topological constraints leads to a statistical-mechanical theory /2,3/ of randomly crosslinked polymer networks which yields an equation for the stress in simple tension in the form

$$\sigma = 2C_1(\lambda - \lambda^{-2}) + 2C_2^*(\lambda^{b/2-1} - \lambda^{-(b+1)}) \quad (1)$$

with

$$2C_1 = \frac{kTM}{V} \quad \text{and} \quad 2C_2^* = \frac{kTN}{V} 6^{-1/2} b \langle R^2 \rangle / \rho_0^2 \quad (2)$$

The C_2 - term describes the departure from phantom network behaviour and results from effects of topological constraints, simulated by a harmonic (EDWARDS-) constraining potential /1/. M is the number of crosslinks in the volume V of the sample and N the number of primary chains in the uncrosslinked polymer from which the vulcanisate is formed. $\langle R^2 \rangle = 1L$ (l - statistical segment length; L - contour length) is the mean-square end-to-end distance of the primary chains, and ρ_0 denotes the mean-square fluctuations of the statistical chain segment after crosslinking. k and T have their usual significance. The parameter b describes the deformation dependence of the mean fluctuations. It has been introduced /2,3/ by the relation

$$\rho_\mu = \lambda_\mu^{b/2} \rho_0 \quad (\mu = x, y, z).$$

In the case $b = 2$ the theory yields a Mooney-Rivlin equation /2/. For crosslinking points per primary chain $M/N \gg 1$ one gets a ratio of the Mooney-Rivlin-parameters C_2/C_1 in the order of unity if $\rho_0^2 \approx 1L$, i.e. mean-square fluctuations in the order of mean dimension of a single macromolecule. Such great values of ρ_0 are in disagreement with calculations made by DOI /4/ for dense polymer systems ($\rho_0^2 \ll 1L$). It was shown that the case $b < 2$ which describes a weaker deformation dependence than the affine ansatz, solves the contradictory /3/.

From a phenomenological point of view TSCHOEGL /5/ proposed a constitutive two-term elastic potential from which eq. (1) could be deduced. The first term is the neo-Hookean potential predicted by the phantom network theory of a "perfect network". The second accounts for contributions arising from "equivalent pseudo-crosslinks" modelling the topological constraints (entanglements) in real rubbers. Reasonable experimental agreement with eq. (1) has been achieved by setting $b = -0.5$ /5/.

The aim of this paper is to outline statistical mechanical considerations for explaining the value $b = -0.5$ and at last to express ρ_0 by chain parameters and polymer density.

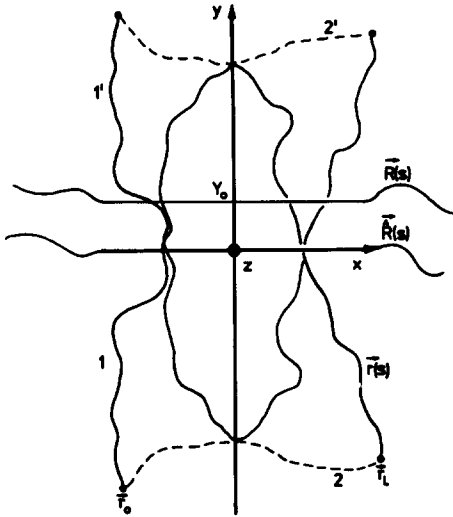
Theory

For simulating the topological constraints of the network chains we present a simple model of an infinite chain hindered by neighbouring chains with endpoints fixed in the gel (crosslinking points). A part of the infinite chain in the mean configuration $\bar{R}(s)$ (s - chain arc length) is approximated by a straight line which we identify with the x-axis of a co-ordinate system (Fig. 1). Further we assume that only such chains are topological active which have endpoints at \underline{r}_{0i} and \underline{r}_{Li} in one half-space $y \geq 0$ and any segment s_i in the xy-plane at $y_i \leq 0$ ("entanglement effects") or $y_i \geq 0$ ("packing effects"). i denotes the chain number. The contribution of the constraining chains to the constraining potential for a segment of the considered chain is supposed to be caused by the differences of their entropy in dependence of configuration $\bar{R}(s)$ of the constrained chain. For simplicity we characterize $\bar{R}(s)$ by the position of the constrained segment $Y(s) = Y_0$.

For a flexible continuous Gaussian chain as a chain model the probability of finding a segment s of a chain with endpoints fixed at \underline{r}_0 and \underline{r}_L in the xy-plane at $y = y$ and $-1/2 \leq x \leq 1/2$ is

Figure 1:

A model for simulating topological constraints.



$$p(y|z_0, z_L) = \int_{-1/2}^{1/2} dz \int_{-1/2}^{1/2} dx p(\underline{r}, \underline{r}_0; s') p(\underline{r}_L, \underline{r}; L-s'). \quad (3)$$

$$p(\underline{r}', \underline{r}''; s'-s'') = \frac{(3/2\pi|s'-s''|)^{3/2}}{(\underline{r}'-\underline{r}'')^2} \exp(-(3/2|s'-s''|) \quad (4)$$

is the distribution function of chain segment distances. For simplicity we replace the x' and z' integrations by

$$1^2 \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \dots \delta(x') \delta(z') dx' dz'$$

and obtain the result

$$p(y|z_0, z_L) = 1^2 (3/2\pi|s'|)^{3/2} (3/2\pi|(L-s'))^{3/2} \exp(-(3/2|(L-s')) (x_L^2 + (y'-y_L)^2 + z_L^2)) \exp(-(3/2|s'|) (x_0^2 + (y'-y_0)^2 + z_0^2)) \quad (5)$$

For the sum of the free energy of the constraining chain with endpoints at x_{oi} , x_{Li} and $-x_{oi}$, $-x_{Li}$ (the corresponding symmetric situation) caused by a displacement of the constrained segment from $Y(s)=0$ to $Y(s)=Y_0$ we obtain

$$\Delta F_i(Y_0 | x_{oi}, x_{Li}) = -T \Delta S_i(Y_0 | x_{oi}, x_{Li}) \quad (6)$$

with the entropy

$$\Delta S_i(Y_0 | x_{oi}, x_{Li}) = S_i(Y_0 | x_{oi}, x_{Li}) + S_i(-Y_0 | x_{oi}, x_{Li}) - 2 S_i(0 | x_{oi}, x_{Li}) \quad (7)$$

$S(Y_0 | x_0, x_L)$ follows from the statistical weight $G(Y_0 | x_0, x_L)$ of the chain with fixed position of endpoints x_0 and x_L via

$$S(Y_0 | x_0, x_L) = k \ln G(Y_0 | x_0, x_L) \quad , \quad (8)$$

and

$$G(Y_0 | x_0, x_L) \sim \int_{Y_0}^{\infty} p(y' | x_0, x_L) dy' \quad (9)$$

From eqn. (5) and (9) one gets

$$G(Y_0 | x_0, x_L) = \text{const.} \exp(-(\alpha/L)((L-s')x_0^2 + s'x_L^2)) \exp(\alpha x^2) (1 - 2/\pi^{1/2} \text{erf}(\alpha^{1/2}(Y_0 - x))) \quad (10)$$

with $\text{erf}(x)$ the error-function, $\alpha = 3L/2ls'(L-s')$ and $x = (y_0(L-s') + y_L s')/L$.

Finally a Taylor-expansion of the error-function up to the second order yields for the free energy in long chain approximation

$$\Delta F_i(Y_0 | x_{oi}, x_{Li}) = kT \ln 6/\pi^{1/2} (3L/2ls_i'(L-s_i'))^{1/2} (y_{oi}/s_i' + y_{Li}/(L-s_i')) Y_0^2 \quad (11)$$

In eq. (11) all terms containing x_{oi} , x_{Li} , z_{oi} , z_{Li} do vanish.

The contribution of all network chains i to the constraining potential is given by

$$\Delta F(Y_0) = \sum_i \langle \Delta F_i(Y_0 | x_{oi}, x_{Li}) \rangle$$

$$= \int d^3 r_0 \int d^3 r_L p^+(\underline{r}_L | \underline{r}_0) p(\underline{r}_0) \Delta F(Y_0 | \underline{r}_0, \underline{r}_L) \quad (12)$$

$\langle \dots \rangle$ denotes averaging over all positions $\underline{r}_{0i}, \underline{r}_{Li}$ of the i -th chain. $p(\underline{r}_0) = \rho_p$ (polymer chain density) is the a priori probability for finding a chain starting point in the gel. $p^+(\underline{r}_L | \underline{r}_0)$ is the probability for finding a chain with starting and end point at \underline{r}_0 and \underline{r}_L and any intermediate point $\underline{y}' > 0$ (configurations 1 and 2' in Fig.1). In accordance with our model we approximate p^+ by

$$p^+(\underline{r}_L | \underline{r}_0) = \int_0^\infty dy' p(y' | \underline{r}_L, \underline{r}_0) \quad (13)$$

with $p(y' | \underline{r}_L, \underline{r}_0)$ from eq.(5). The appropriate probability for the symmetric configurations 1' and 2 (Fig.1) can be written as

$$p^-(\underline{r}_L | \underline{r}_0) = \int_{-\infty}^0 dy' p(y' | \underline{r}_L, \underline{r}_0) .$$

Performing the integration yields

$$\begin{aligned} p^+(\underline{r}_L | \underline{r}_0) &= l^2/2 (3/2\pi lL)^{5/2} L^2/(s'(L-s')) \\ &\exp(-(\alpha/L)((L-s')\underline{r}_0^2 + s'\underline{r}_L^2)) \exp(\alpha x^2) \\ &(1 - (2/\pi^{1/2})\text{erf}(-\alpha^{1/2}x)) . \end{aligned} \quad (14)$$

This probability depends only on the permanent topological situation (i.e. is independent of external deformation /1/) which is fixed after the vulcanisation process. If long constraining network chains are assumed, the probability p^+ is nearly the same for all s' and the constraining segment can be assumed to be $s' = L/2$.

The free energy difference $\Delta F(Y_0)$ in the deformed state depends on the deformation by the displacement of the endpoints of the constraining chains. If we assume an affine displacement of the crosslinks,

$$\underline{r}_{0i} \longrightarrow \underline{\lambda} \underline{r}_{0i} , \quad \underline{r}_{Li} \longrightarrow \underline{\lambda} \underline{r}_{Li} , \quad (15)$$

we obtain from eqn. (12) and (14) after expanding the error-function (for $y_0, y_L \gg (lL)^{1/2}$ the integrating function gives extremely small contributions to the integral) the free energy per constrained chain arc length

$$\Delta \tilde{F}(Y_0; \lambda) = \Delta F(Y_0; \lambda) / l = kT \frac{8^{3/2}}{3\pi^{1/2}} \frac{l^{1/2}}{L^{1/2}} \rho_p \lambda_y Y_0^2. \quad (16)$$

Using the diagonal form of λ in (15) is in accordance with the assumption of the EDWARDS-theory /1/ that the constraining potential is independent from the direction of the constrained segment.

A generalization of eq. (16) then gives

$$\frac{\Delta \tilde{F}}{kT} \sim \rho_p (\lambda_x (X-\hat{X})^2 + \lambda_y (Y-\hat{Y})^2 + \lambda_z (Z-\hat{Z})^2) \quad (17)$$

with $\hat{R} = (\hat{X}, \hat{Y}, \hat{Z})$ the mean configuration and $R = (X, Y, Z)$ the actual configuration of the constrained chain.

From eqn. (16) and (17) and from eq. (20) in /2/,

$$\frac{\Delta \tilde{F}(\lambda)}{kT} = \sum_{\substack{\mu= \\ x,y,z}} \frac{1}{\rho_\mu^4(\lambda_\mu)} (R_\mu - \hat{R}_\mu)^2,$$

follows

$$\rho_\mu \approx 0.9 q^{1/4} (lL)^{1/2} \lambda_\mu^{b/2}; \quad q = \frac{v/N}{(lL)^{3/2}} \quad (18)$$

with $b = -0.5$, i.e. the value of the TSCHOEGL-equation.

Discussion

The presented model must be regarded as a simple attempt to simulate chain constraining effects. Nevertheless it gives a proper result concerning the deformation dependence of the constraining entropic potential which is in agreement with experimental observations /5/. In this sense the $b=-0.5$ result gives a support of the network theory in /2,3/, especially for the statistical interpretation of the Mooney-Rivlin-like behaviour of the tensile stress.

Eq. (16) indicates that in good approximation the constraining potential is a harmonic-like. This confirms the idea of the tube-like confinement /6,7/ due to the topological restrictions that chains cannot pass through each other. EDWARDS and DEAM /8/ argued that the density of entanglements dominates

the tube radius ρ_0 . Our model indicates that both "entanglement effects" and "packing effects" give contributions (but with different weight) to the constraining potential.

The estimation of the tube-radius is one important problem in the field of concentrated polymer solutions and several attempts have been made to calculate it in terms of a harmonic potential /1,4,9,10/. Though EDWARDS /1,10/ and DE GENNES /9/ used different approaches, they reached the same result for an uncrosslinked concentrated polymer solution, namely $\rho_0 \sim \rho_p^{-1/2}$. DOI /4/ criticized this result using scaling requirements which should be satisfied in the continuous Gaussian chain model. He found $\rho_0 \sim \rho_p^{-1}$ under the conditions $(lL)^{3/2} \gg \rho_p^{-1}$ and $\rho_p l^2 L \ll 1$ which should be realized at very large degrees of polymerization. We note that the result $\rho_0 \sim \rho_p^{-1/4}$ (eq. (18)) gives support for BUECHE's relation $n_c \sim \rho_p^{-1}$ /11/, where n_c is the critical degree of polymerization below which the tube-model breaks down and which is defined by $l n_c^{1/2} / \rho_0 = \text{const.}$ Using eq. (18) this relation yields the ρ_p^{-1} dependence.

It is interesting to note that the tube-like model can be reformulated in the frame of the primitive chain concept /12/ in which is assumed ρ_0 to be equal to the average length of a primitive chain step at equilibrium. In this model the calculation of ρ_0 in /13/ yields $\rho_0 \sim \rho_p^{-3/4}$ using the scaling concept (DE GENNES /14/) in polymer physics and $\rho_0 \sim \rho_p^{-3/5}$ /12/, respectively, using a mean-field theory. DOI and EDWARDS /12/ argued that a deformation modifies the tube only longitudinally but not transversally. The different assumption of changing the tube diameter by external deformation, proposed by MARRUCCI et.al. /15,16/, is in principle agreement with our result.

Further, we note that the presented model gives hope for explaining the relaxation behaviour of the Mooney-Rivlin parameters /17/. The "fast" relaxation of C_1 after a sudden deformation may be explained by the balancing process of tensile forces acting on the primitive subchains /12/. On the other hand, the "slow" C_2 relaxation may be expected to be determined by a segment diffusion process (may be a partial reptation diffusion) which forces the distribution of segment position around \bar{R} after deformation to the new equilibrium distribution.

We note finally that the characteristic swelling behaviour of polymer networks (decreasing C_2 -value

with increasing degree of equilibrium swelling) may be explained in a natural manner. There are two effects causing the swelling result. First, the increase in the ρ_0 -dimensions, and second, the loosening from the condition that crosslinks are embedded in the network structure (condition of fixed end-points) and hence a loosening from the assumption of affine displacement of junctions under strain /18,19, 20/. Considerations under this viewpoint are in progress.

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